

Mechano-sorptive creep of Portuguese pinewood chemically modified

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SUMMARY

The effect of chemical modification on mechano-sorptive creep in bending was studied by experimental work. Stakes with $20 \times 20 \times 400$ mm RTL of Portuguese wood species (*Pinus pinaster* Aiton) modified with 1,3-dimethylol-4,5-dihydroxyethyleneurea (DMDHEU), m-methylated melamine resin (MMF), tetraethoxysilane (TEOS) and amid wax (WA) were measured under asymmetric moistening conditions over a period of 42 days (app. 1000 hours) with stress level (SL) of 12 MPa, according to ENV 1156.

The cell wall treatments (DMDHEU and MMF resins) had shown significant reduction of creep (creep factors, k_c) when compared to untreated wood under similar conditions. Both types of resins and levels of treatments (different WPG) did not shown significant effects.

In the lumen fill treatments, deposit material of TEOS did not affected the creep behaviour (k_c); Wax treatment was shown a particular compliance of creep due to avoid exchange moisture (by the hydrophobic effect of wax).

The anti-creep efficiency (ACE) correlated better than other mechanical or physical properties imparted by the modification process.

KEY WORDS

amid wax, bending creep, creep factor, mechano-sorptive effect, *Pinus pinaster*, resins

INTRODUCTION

The creep propensity is an important quality parameter for wood used as load-bearing material in building constructions. The wood-moisture interaction has a decisive role on the behaviour of a horizontal member in loaded condition, where long-term deformation occurs. The mechano-sorptive effect (MSE) is an amplification of the elastic deformation and an acceleration of the visco-elastic strain rate.

Over the last years an extensive work on quantifying and predicting creep behaviour has been undertaken: in untreated wood (Hoffmeyer and Davidson 1989; Morlier 1994; Bengtsson 2001; Hunt 2004), wood products (Dinwoodie et al. 1981; 1984; 1990; 1991a; 1991b; 1992) and modified wood (Norimoto et al. 1992; Epmeier and Klinger 2005). In the latter's, some of the most important parameters and characteristics of mechano-sorptive behaviour are as follows:

- Treatments with cell wall reaction (especially resin based) had good relation with moisture-change. They assumed the best performance under the creep of MSE.
- Modification of the cell wall at the molecular level (and not filling the cell-wall cavities alone) was required to affect the MSE.
- The effect of chemical modification on the MSE of wood creep can be characterized by a factor named anti-creep efficiency (ACE) which has a good correlation with anti-swelling efficiency (ASE).

Creep results might be affected by different variables: tree rings width, provenance material in the tree and stem, close to the pith or to the bark (Bengtsson 2000, 2001), modulus of elasticity (MOE), ratio volume and cross section area (V/A), environment temperature (Green and Evans 2008), historical load (due to the cumulative effect), drying type (Hanhijärvi 1999) and moisture content (MC) (Hering and Niemz 2011). The wood material heterogeneity does not allow different variables of material to reflect alone on the creep results. However, it's unanimously accepted that the wetting and dry changes of wood material is the highest amplifier of the creep deformation (Norimoto et al. 1992; Bengtsson 2000; Hunt 2004; Epmeier et al. 2005).

Logsdon (1998) studied separately the compression and tension strength behaviour with different range of MC, indoor up to fibre saturation conditions. While the compression strength showed a reduction up to 80%, tensile stress reduced up to 40% (comparatively, fifty percent less). Bengtsson (2000) had showed larger creep effect in compression than in tension under unidirectional MSE of untreated pinewood.

Under asymmetric moistening conditions in bending, compression zone showed larger deformation than in tension wet, at indoor creep or mechano-sorptive conditions, respectively by Moliński and Raczkowski (1988) and Roszyk (2005).

This study was conducted in bending under asymmetric moistening conditions, with compression and tension zone. The reasons to support this decision were related to the enhancement of mechanical properties imparted by the chemical modification and practical applications, briefly described as follows:

- Treatments with good relation with moistening (Pfeffer 2011), the cell wall reaction treatments (DM-DHEU and MMF resin) had shown significant in-

creasing on the compression strength and decreased in the tension strength in different extend (Bollmus et al. 2009).

- Bearing elements working in the so-called semi-open space, condensed water vapour falling on wooden materials and leaking roofs leading to seepage on rafter framing are practical examples to pursue this study.

The objective of this work is to study the mechano-sorptive creep behaviour in bending of Portuguese modified pinewood under asymmetric conditions of moistening.

MATERIAL AND METHODS

Four methods of chemical modification were investigated: 1,3-dimethylol-4,5-dihydroxyethyleneurea (DM-DHEU), N-methylol melamine (MMF), tetra-alkoxysilane (TEOS) and amid wax (WA).

The specimens were dried for 24 h at 103°C and then impregnated with different solutions. A full cell process with a vacuum step of 30 min followed by 2 h pressure step at 12 bar were used.

Impregnations with aqueous solutions of DM-DHEU supplied by BASF (Ludwigshafen, Germany) were performed in the following concentrations: 1.3 M and 2.3 M using 4% magnesium nitrate relative to the mass of DMDHEU of the solution as catalyst. Two levels of modification with DMDHEU resin are referred as D1 and D2.

N-methylol-melamine formaldehyde (MMF) was Madurit MW 840 supplied by INEOS (Frankfurt a. M., Germany). The original resin/water solution had 75% of concentration. To obtain two levels of concentrations (15 and 30%) it was diluted with water. After impregnation, specimens were dried for 48h at room temperature. For resin curing, wood material was stored four days in an oven with 5 steps of temperature. Until reach 90°C, the temperature increase 10°C every day. Two levels of modification with MMF resin are referred to hereinafter as i1 and i2.

TEOS was applied in sol state as described by Donath et al. (2004). Ethanol (1 mol) was added to 1 mol and stirred at ambient temperature for 30 min. After the impregnation, specimens were cured in an oven at 60°C for 4 days. TEOS treatment is abbreviated as T.

A synthetic amid wax in hot melting state was used. The wax was impregnated at temperature of 120°C in liquid state. The modification with amid wax is abbreviated as WA.

Additional information about treatments used in this study can be found in different works, Militz (1993); Epmeier et al. (2004); Donath et al. (2004) and Scholz et al. (2009), respectively.

All works were made using Portuguese maritime pine specie (*Pinus pinaster* Aiton) with pure sapwood part of the stem. Specimens were cut carefully, so that each one would contain the same annual rings and would be exactly straight-grained with dimensions $20 \times 20 \times 400$ mm RTL resulting in a total of 129 specimens, i.e. 31 controls and 98 modified specimens.

Density of the tested wood was determined at indoor conditions of moisture content (RH 50%) before modification, was within the range of 520 to 550 kg/m³. The orientation of the growth rings of wood specimens was parallel to its faces and perpendicular to the support. The width of annual rings was about 3 mm on tile average, see grey lines in fig. 1B.

The load was applied in a four-point bending system (4 pb) according to EN 408 and ENV 1156, fig. 1A. Supports were spaced at 360 mm and loading blocks (16 kg/157 N) were spaced at 180 mm and selected in such a way to ensure constant loading with 12 N/mm² in bending stress ($>12\%$ of modulus of rupture for untreated wood, MOR).

Two moistening process were applied separately, see fig. 1A. In the first case, moistening was carried out on the upper compression stress side. In the second one, the tensioned fibres were as well in the upper side. In this case, the support and load-shoes positions were changed.

The moistening was achieved by fixing strip filter paper to the radial surface, on top of the specimen, stretched in the middle part of 180 mm (between load-shoes) and whose ends were dipping into a container to adsorb water by capillarity (over 5 hours long). The moistening processes were initiated after seven days/first week of loading and repeated every week until 5 cycles were reached (42 days /1000 hours).

Twenty millilitres of distilled water with 5 hours of expositions in the upper radial surface of the specimens were used. This environment conditions are similar to the Mediterranean climate in the southern Europe, moistening variation by a downpour and the remaining weeks with low RH happened very often.

The length of the cycle was defined with a preliminary evaluation of moisture content (MC). Unloaded specimens under similar conditions of moistening as the creep test were used. Afterwards, the moisture content was measured at different times with a Protimeter Moisture Measurement System (Instruction Manual Protimeter 2005). Two pins were pressed against to the tangential surface of wood specimen with few millimetres (2–3 mm) of penetration. After few seconds, the MC was obtained in 3 depth, according to fig. 1B. The average of both sides of the cross section was taken.

Tension and compression strength in the longitudinal direction were performed on a Zwick/Roel ZMART. PRO 100 kN test machine (Ulm, Germany).

Table 1 shows a summarized an overview of different properties, specimens sizes and applied standards followed in the experimental work.

Dynamic MOE_{dyn} tests were carried out using the impulse vibration technique. The specimens were placed on foam rubber to simulate the free-free condition with respect to axial vibration ($0.224 \cdot l$, where l is

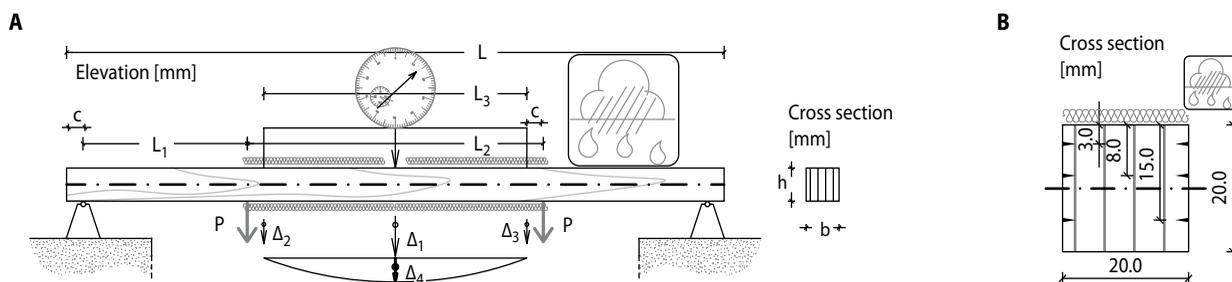


Fig. 1. A – Load and moistening arrangement for 20·20·400 mm³ RTL specimen, B – Local measurements of moisture content in the cross section at different depth from the radial surface wetted (3, 8 and 15 mm)

the specimen's length). A hammer then excited the axial vibration of the specimens. The sound pressure was registered via a microphone connected to a computer-based data acquisition system. The frequency spectrum was established from the sound pressure using Fast Fourier Transformations (FFT) and the eigen-frequency was determined from the appropriate peak. Based on eigen-frequency f [Hz], length l [m] and density ρ [kg/m³], the MOE was calculated as follow:

$$MOE_{dyn} = 4 \cdot \rho \cdot f^2 \cdot l^2 \text{ [kN/mm}^2\text{]} \quad (1)$$

Tab. 1. Properties, sample size LRT in mm, applied standard and number of specimens (n) per treatment

Strength property	Assignment	Specimen (mm ³)	Standard	n
Parallel compression ^a	$f_{c,o}$	30 × 20 × 20	DIN 52 185	10
Parallel tension ^a	$f_{t,o}$	300 × 20 × 15	DIN 52 188	20
Modulus of elasticity ^b	$MOE_{st,4pb}$	400 × 20 × 20	EN 408 ^e	20
Modulus of elasticity ^c	$MOE_{st,3pb}$	400 × 20 × 20	DIN 52 186	10
Modulus of elasticity ^d	MOE_{dyn}	400 × 20 × 20	–	20
Modulus of rupture ^b	MOR	200×10×10	DIN 52 186	10
Moisture content	MC	400×20×20	Protimeter	5

^a Zwick/Roel ZMART.PRO 100kN test machine (Ulm, Germany); ^b and ^c Zwick/Roel ZMART.PRO 10kN test machine (Ulm, Germany); ^d Grindosonic MK5 (J.W.Lemmens N.V.; Leuven; Belgium); ^e creep test according to ENV 1156.

The ACE is determined according to the following equations:

$$ACE = (dJ_u - dJ_t)/dJ_u \cdot 100 \text{ [%]} \quad (2)$$

$$dJ_i = 2 b h^3 / 3 P L_1 L_3^2 (\delta_2 - \delta_1) \text{ [MPa}^{-1}\text{]} \quad (3)$$

where:

- dJ_i – the creep compliance with $i = u$ or $i = t$,
- dJ_t – the creep compliance for treated timber,
- dJ_u – the creep compliance of untreated timber,
- P – the applied load,
- δ_2 – the deflection after 42 days,
- δ_1 – the deflection after 60 s loading,

- L_3 – the gauge length for the determination of $MOE_{st,4pb}$,
- L_1 – the span between support and load,
- $bh^3/12$ – the moment of inertia of the cross-section.

The bending deflection was measured from the top surface of the specimen at mid-span with 160 mm span using lvdt gauges and recorded with PC-based Data logging procedure automatically at 5 s time intervals (for the first 4 hours) and at each 30 minutes for the next days. The same procedure was repeated every week cycle.

The relative creep (ϕ_t) was calculated as the deflection at a specific time divided by the deflection after 60 seconds (δ_0). The creep factor (k_c) was calculated as the increase in deflection with time (δ_c) divided by the initial elastic deflection, after 60 s. Where δ_t is the deflection at time t and ϕ_t is the relative creep at time t :

$$k_c = (\delta_t - \delta_0)/\delta_0 = \delta_c/\delta_0 - 1 = \phi_t - 1 \quad (4)$$

For comparative analysis of creep results (relative creep with time, Φ_t) the power function model (PFM) with three coefficients was used:

$$\Phi_t = \beta_0 + \beta_1 \cdot t^{\beta_2} \quad (5)$$

where β_0 represents the instantaneous elastic deformation and can be calculate from the MOE and the size of the specimens for any given load, according to the material behaviour:

$$\Delta_4 \cong 3 P L_3^2 L_1 / (4 b h^3 E) \quad (6)$$

where:

- P – the load at each side,
- L_1 – the span between load-shoes and support,
- E – modulus of elasticity,
- L_3 – the span where the curvature where measured.

The second term $\beta_1 \cdot t^{\beta_2}$ of the PFM is the creep deflection. The parameters β_1 describe the slope of the relative creep curve and β_2 is the power factor that translate the influence of time. This second term grows with time approaching an asymptotic limit.

RESULTS AND DISCUSSION

All studied properties of untreated and modified wood were characterized by mean value (\bar{x}), median (horizontal line in the box plot) and standard deviation (box).

The whisker plots displayed the 5 and 95% percentile range. For comparative purposes, a t-test analysis was carried out to verify whether a change was significant. The level for significance was set at $p < 0.05$.

For fitting creep curves and forecasting data, the ORIGIN statistical software was used. For unconstrained models, the default algorithm used by ORIGIN is the Gauss-Newton method of finding the minimum of function that is a sum of squares of non-linear functions.

Moisture content distributions

To check the MC distributions in the cross section, a preliminary experiment was done where allowed clarifying some doubts:

- The first one, it was an attempt to establish the length of the cycle for the creep test duration, in a way to reach the wood stabilization after the wet and dry cycle.
- The second one, it was how far the moistening process is suitable to produce a MC changing. Special care had taken in the study of modified specimens.
- The last ones were checked the MC above and below of the neutral axis (n.a.). Which level of MC was reached with this asymmetric moistening procedure above the n.a. whilst below n.a., no changes were expected.

Figure 2 shows the means values of MC distribution on the specimens cross section during their moistening at different depth, see also fig. 1B).

Below the n.a. the MC was not affected by the moistening. However above n.a. both materials stud-

ies (control pinewood, in the fig. 2A and DMDHEU treated wood, in the fig. 2B) had reached similar MC to the EMC found in the wetted stabilized conditions, RH of 87%. Only one part of the cross section (up to the n.a.) changed the MC in a way to produce the mechano-sorptive effect.

Resin based treatment took up to five days to reach and stabilize the preliminary EMC, before moistening. On the other hand, untreated pine took up to three days to stabilize, despite higher MC was reach. One week for the length of cycle in the MSE in bending creep was taken.

Protimeter MMS moisture-meter was able to access the MC in the pine wood and other species well identified. Therefore, it is not appropriated to access directly the MC in the modified wood with DMDHEU resin, despite similar density was used. The found MC should be considered a rough approach.

In the literature, Pfeffer (2011) with untreated Scots pine and resin based treatment (DMDHEU) had shown significant correlations between the MC measured by gravimetric and by electrolyte method.

Mechanical properties

Figure 3 shows different enhancement on the strength properties in the modified pinewood. Compression strength parallel to the grain increased significantly for resin based treatments, with large extend in DMDHEU than MMF resin.

In the Lumen fill treatments, TEOS had no effect and wax had shown a slight increased, up to 15%, fig. 3A).

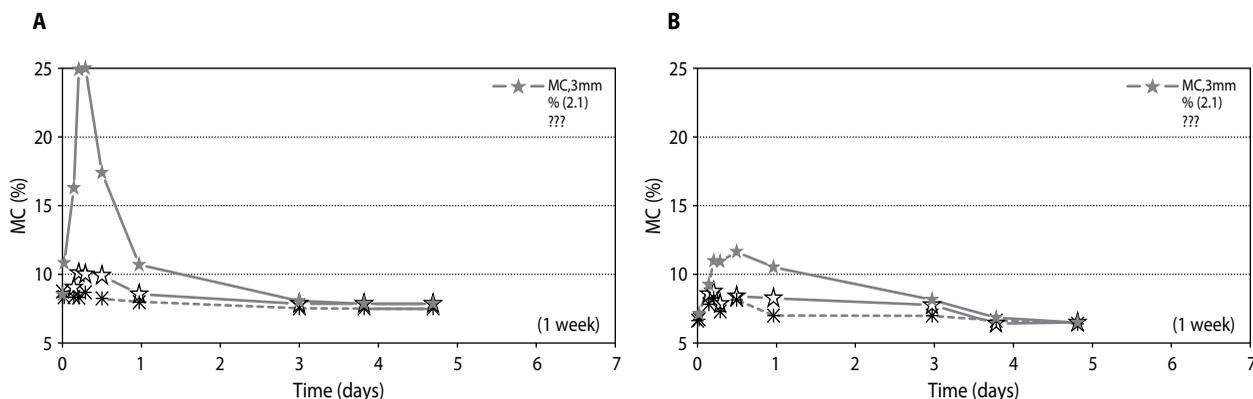


Fig. 2. Profile of the moistening the top radial surface, A – untreated pinewood and B – DMDHEU (D1, 15% WPG) (★ 3 mm; ☆ 8 mm and * at 15 mm, see also fig. 1B)

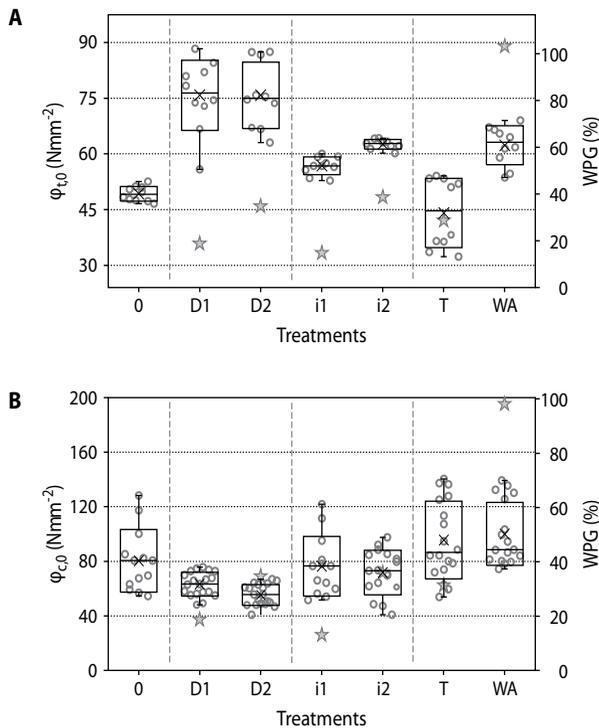


Fig. 3. A – Compression strength; B – tension strength and WPG (★). For abbreviation see material item

Tension strength parallel to the grain acted in the same way for lumen fill treatments, but in the other way around resins based treatments. High concentration of DMDHEU resin (D3, 35% WPG) was reduced up to 25%. In the remaining resin type and concentrations as well in the lumen fill treatment (TEOS and wax) did not shown a significant effect despite the WPG observed, fig. 3B.

The hardness increase and the embrittlement effect of the cell wall reaction are the main contributor to this behaviour (Rowell 1996; Mai et al. 2007; Xie et al. 2007).

For both moistening setups done at 12 N/mm² of stress level no failures were occurred.

Wetted compression zone

Figure 4 shows some of the compliance curve of relative creep in four points bending (4 pb) according to EN 408 and ENV 1156 when the moistening process was done in the compression zone.

In all specimens, cells wall reaction treatments (DMDHEU and MMF resins), TEOS and untreated specimens, an increasing of moisture content means a creep deflection variation. Therefore, drying process

tends to have a different displacement recover between cell wall reaction and lumen fill treatments. At the 2nd days of the cycle, untreated wood and TEOS treatment had shown stabilized creep deflection. In the resin based treatments, the stabilization deflection took place at the 4th up to 5th day of the cycle.

To represent the mean deflection and achieved the mean relative creep, the compliance creep curves obtained from creep tests were fitted by power function model – PFM. The PFM is designed to fit primary creep and does not include a term that would indicate the possibility of accelerated creep to failure.

The slope of the fitting curve translates the creep limit which has a particular interest to analyze and compare the creep behaviour (Hunt and Shelton 1988). Mohager and Toratti (1993) had shown no creep limit with different size specimens of untreated Scots pine under MSE over long-term (8 years). That means, with successive wetted and dry cycles, the creep deformation is unstable or increases indefinitely.

Between modified wood with resins (DMDHEU and MMF) and untreated wood, the difference of the slope creep curves was clearly. One possible explanation is that moisture in untreated wood acts as a plasticizer (Holzer et al. 1989), i.e. the deflection increases with increasing moisture content as a result of MC and MOE variation. Modified wood with resin based had shown the same trends with moistening in the stiffness stabilization efficiency (SSE) and (ASE) anti-swelling efficiency (Norimoto et al. 1992; Epmeier et al. 2005).

In the beginning of each cycle of untreated wood creep, the wetting causes swelling and concomitantly a larger moment of inertia responsible for the negative peak of deflection. The first adsorption causes an increase in deformation in different extend from the next ones. The following adsorption cycles had caused an increase deflection in the less extend, see fig. 4A. Modified wood had shown the same instability with less extend between the first and next cycles. The best performances of resins based treatments in ASE and SSE help to explain its lesser extent (fig. 4B and C).

Figure 5 shows the relative creep for wax specimens tested under similar moistening process in the compression zone than control and resin based treatments. The wax treatment had shown a hydrophobic behaviour. For that reason no experiment with wax were done in the tension zone moistening. The hydrophobic effect of the wax

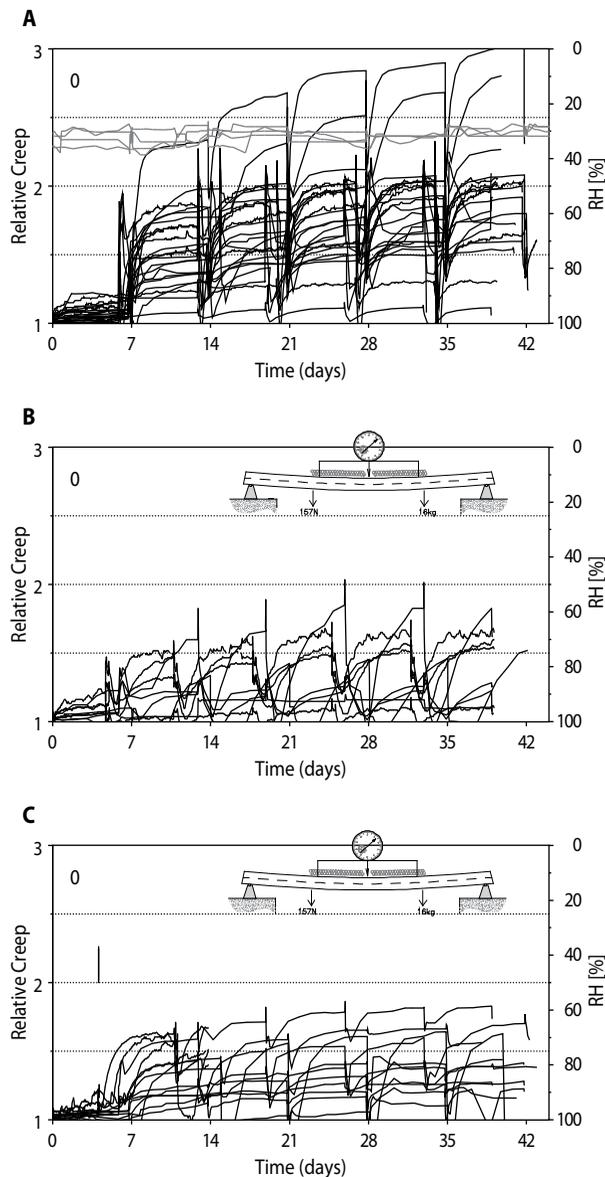


Fig. 4. Compliance curves of relative creep and RH environment conditions for pinewood A – 0 *ctrl*, B – DMDHEU (1.3M, 18% WPG) and C – MMF (16% WPG)

and the slower water penetration presented by Scholz et al. (2009) with similar wax, can be explained the creep behaviour of wax treatment. The evaporation took place first then the capillarity water uptake/absorption into the wood material. The sealer effect of wax did not let shown the mechano-sorptive effect. Actually, the MSE doesn't judge completely eradicated in the wax treated wood. However, surround environment change will have a less effect and move forward with phase. This means,

when the wood start to wet the surround environment conditions start to dry. It is credible for practical applications that the wax in lumen of the cell wall avoids the water circulations through the wood material.

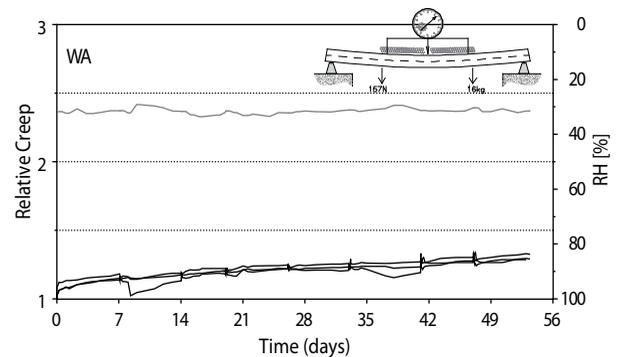


Fig. 5. Compliance curve of relative creep and RH environment conditions for pinewood treated with wax (95% WPG)

Wetted tension zone

Figure 6 shows the compliance curve of relative creep with moistening process in the tension zone. As in the compression zone wetting process, untreated wood had shown no creep limits. In the other hand, modified wood had shown less amplitude than untreated wood behaviour and a constant balance. At the end of the experiments (42 days/1000 hours), the slope or the creep limits can be translate by k_c factor, see fig. 7B.

Figure 7 shows the creep factor (k_c) over 42 days/1000 hours and 5 wet/dry cycles. For both process of moistening, k_c were obtained from the mean relative creep curves fitted with PFM following the eqt. 5. Resin based treatments had shown similar behaviour and less creep than untreated wood. In the lumen fill treatments, TEOS had shown no effect and wax treatment had shown a particular effect.

In the modified wood with resin based treatments, fitting curves of relative creep had shown lower and less scattered creep factors (k_c) at 42 days forecasting.

Whilst in the lumen fill treatment (TEOS) the creep factor (k_c) did not shown any difference to untreated pinewood.

Under uniform changing of RH environment (30 and 90%), Mohager and Toratti (1993) with small specimens $10 \times 10 \times 330$ mm RTL of Scots pine had found a creep factor of 1.05. In the same conditions but with

specimens with full scale dimensions 1 : 1, Toratti (1993) was shown an increase of creep factor app. 0.80. Epmeier (2006) conducted a study with a large and well-documented provenance specimens with full scale 1 : 1 and showed a range creep factor between 1 to 1.35. Bengtsson (2001) with untreated wood from different positions of the stem (heart and sapwood) and type of tree (fast and slow growth) showed a range of creep factor between 0.9 up to 1.57.

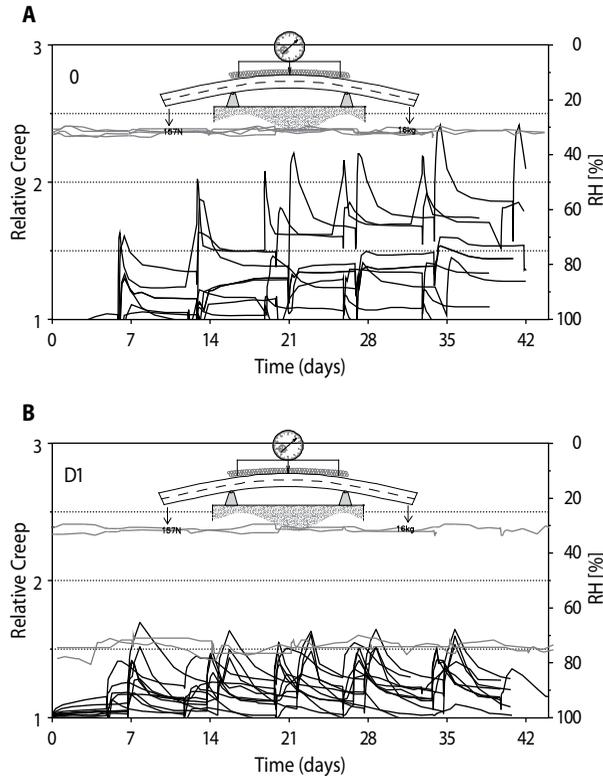


Fig. 6. Compliance curve of relative creep for A – untreated pinewood, 0 ctrl and B – DMDHEU (1.3M, 18% WPG) and RH conditions

In this study of the MSE in the tension moistening zone with untreated pinewood had shown similar results than Roszyk (2005). He worked with Scot pine pure sapwood and similar setup, a mean value of creep factor up to 0.80 was shown.

Our results of the creep factor for the MSE with short dimension specimens 1 : 10 became in line with literature results for other pines in full 1 : 1 or small 1 : 10 scale specimens.

The MSE in the unidirectional tension creep is less than in compression with ratio 1 : 2 (Bengtsson 2000).

Comparatively, the mechano-sorptive in bending with 4 pb of untreated pinewood had shown lower creep factor for tension than compression zone moistening (15%). Similar bending setup for tension and compression together, Roszyk (2005) had shown means creep factor 35% less in tension moistening zone. The difference between both results can be explained mainly for two reasons: The ratio V/A exposed to the moistening and the stress level 50% higher, 18 N/mm². Schniewind (1967 and 1968) suggested that a lower value of the ratio V/A, the higher pronounced of MSE is.

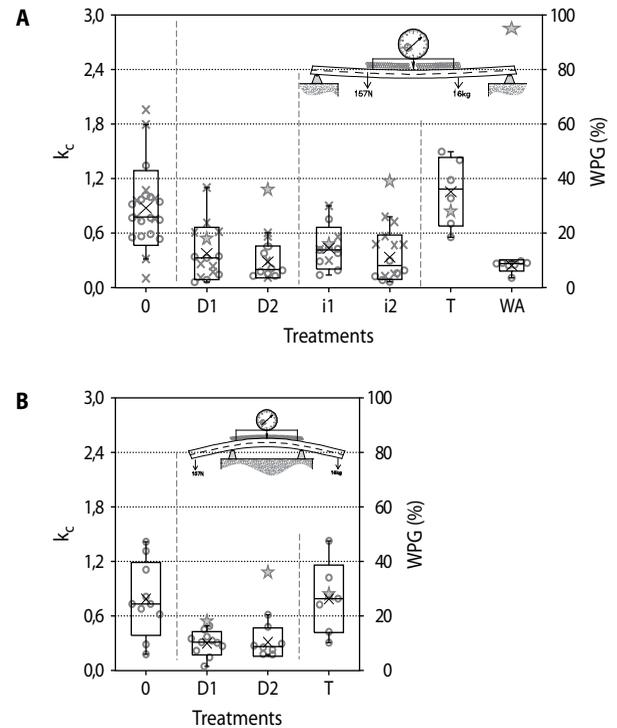


Fig. 7. Creep factor (k_c) over 42 days with wetting at, A – compression zone and B – tension zone with 4pb and WPG (★). For abbreviation see the material item

Table 2 shows the creep factor in the MSE for both moistening setups in compression and tension zone.

Modified wood with DMDHEU resin did not shown significant difference between both setups. Lumen fill treatment (TEOS) had shown a creep (%) factor (k_c) 20% lower in tension moistening.

Over 42 days with 5 wet and dry cycles, modified wood with resin based (DMDHEU and MMF) had shown a significant reduction on the creep factor (k_c) greater than 50%, see also figure 7A. MMF with

lower concentration (i1) had shown less reduction than DMDHEU resin.

Tab. 2. Mean of creep factor (k_c) and difference between modified wood and untreated with [non significant values]

Wet / Treatment	0-ctrl	D1	D2	i1	i2	T	WA
$k_c (f_{c,o})^a$	0,89	0,33	0,28	0,41	0,29	1,05	0,24
Difference [%]	–	–63	–69	–54	–68	+18	–73
p-value	–	0,00	0,00	0,00	0,00	[0,32]	0,00
$k_c (f_{c,o})^b$	0,79	0,30	0,31	–	–	0,79	–
Difference [%]	–	–62	–60	–	–	+0,08	–
p-value	–	0,01	0,01	–	–	[0,77]	–

^a Creep factor with moistening in the compression zone;

^b moistening in the tension zone of bending creep test over 42 days/1000 hours according to ENV 1156.

Both levels of DMDHEU modifications (D1 and D2 with 18 and 36% WPG used in this study) had shown a slight decrease in the creep factor, up to 2%. This result has an important meaning in the industrial scale of chemical modification where the dimension specimen plays an important role. Wood with large cross section has the propensity to establish internal chemical gradient. Homan and Bongers (2004) had shown a gradient of app. 50% with uneven chemical distribution in the cross section (greater than 50 mm). Epmeier and Kliger (2005) with full scale specimens modified with both concentrations of MMF treatment (with 7.5 and 15%) had shown no significant difference in the MSE of bending creep. Similar results, with no significant difference, were shown in this study with MMF (with 15% and 30% concentration). A minimum level and sufficient cell wall modification are required to achieve the enhancement of the MSE on the bending creep.

Furfurylated wood is a similar treatment to the DMDHEU resin with high concentration. Epmeier et al. (2007) with furfurylated specimens in full-scale 1 : 1 under symmetric moisture change found a creep factor up to 75%.

DMDHEU resin had shown a mean value up to 30%. The ratio V/A exposed to the moistening and setup used should be the main reasons to justify both results.

In this study, MMF with medium concentration had shown similar creep factor (up to 41%, mean value), as Epmeier and Kliger (2005) and Norimoto et al. (1992)

with similar concentration. Despite, differences in the setup and V/A ratio of specimens, respectively with full scale 1 : 1 (k_c 47% of creep factor) and the latter authors with small scale 1 : 15 (mean value of creep factor, up to 40%).

Under different set up conditions but with acetylated wood, the latter's authors found similar creep factor, up to 30%.

Correlation analyses

Several authors correlate the stiffness (short-term properties) or the wood quality (MOE/density) to the long-term performance in the creep test of untreated wood (Hoyle et al. 1985; Bengtsson 2001). Epmeier et al. (2007) corroborated the later results for Scots pine but had found minor correlation in the modified wood, i.e. acetylation, MMF, heat treatment in oil bath and furfurylation.

The density is an important wood feature and often regarded as being closely related to deformation (or resistance). Table 3 shows different correlation between Density, stiffness and deformations found in the creep tests. As far as untreated wood were concerned moderate up to significant correlation were found.

In the modified specimens, despite few specimens tested (seven) in the lumen fill treatment (TEOS), the tendency of correlation remained between density and other properties.

In the cell wall treatments (DMDHEU and MMF resins) the correlations in the most cases were lower. Occasionally significant correlations were found, but not confirmed in other concentrations or similar treatments.

As a summarizing, the prediction of performance criteria based exclusively on density should not be formulated for modified wood. Although, in the stiffness accessed with vibration technique (MOE_{dyn}) for untreated and treated wood with high concentration of resin (DMDHEU and MMF) significant correlations were found.

Correlation between creep deflection and relative creep is moderate for the untreated control and DMDHEU (D1, with medium concentration) and significant for DMDHEU (D2, with high concentration), MMF and TEOS.

Despite the particular hydrophobic behaviour of the wax treatment no significant correlation were found.

Tab. 3. Coefficients of correlation for modified wood specimens and untreated pine at each moistening process, [non-significant values] in brackets. For abbreviations see the material item

Treatments			0	D1	D2	i1	i2	T	WA
$f_{c,o}$ wetted Compression side									
Density	vs.	MOE _{dyn}	+0.69	[+0.10]	+0.61	[+0.07]	+0.60	+0.56	[+0.37]
Density	vs.	MOE _{st,4pb}	+0.77	[+0.30]	[+0.50]	[0.32]	[+0.47]	[+0.11]	[+0.28]
Density	vs.	MOE _{st,3pb}	+0.69	[+0.14]	[+0.4]	[+0.54]	+0.56	+0.91	[+0.33]
Density	vs.	relative creep	-0.86	[-0.05]	[-0.54]	[-0.25]	[-0.18]	-0.78	[-0.02]
Density	vs.	creep deflection	-0.70	[-0.01]	[+0.15]	[-0.42]	[-0.26]	-0.68	[-0.44]
Creep deflection	vs.	relative creep	[+0.43]	[+0.35]	+0.74	+0.64	+0.62	+0.85	[+0.01]
Creep deflection	vs.	MOE _{st,4pb} /DEN	[-0.33]	[-0.45]	[-0.36]	[-0.48]	[-0.18]	[-0.26]	-0.80
Creep deflection	vs.	MOE _{st,4pb} *	-0.67	[-0.35]	[-0.54]	-0.80	[-0.35]	[-0.39]	[-0.37]
$f_{t,o}$ wetted Tensile side									
Density	vs.	MOE _{dyn}	+0.67	[+0.24]	[+0.32]	-	-	+0.84	-
Density	vs.	MOE _{st,4pb}	+0.78	[+0.09]	[+0.14]	-	-	+0.60	-
Density	vs.	MOE _{st,3pb}	+0.73	[+0.16]	[+0.11]	-	-	+0.68	-
Density	vs.	relative creep	-0.72	[-0.01]	[-0.04]	-	-	-0.64	-
Density	vs.	creep deflection	-0.63	[-0.11]	[+0.04]	-	-	[-0.42]	-
Creep deflection	vs.	relative creep	[+0.54]	+0.64	+0.81	-	-	+0.56	-
Creep deflection	vs.	MOE _{st,4pb} /DEN	-0.84	[-0.08]	[-0.04]	-	-	[-0.49]	-
Creep deflection	vs.	MOE _{st,4pb}	-0.62	[-0.48]	[-0.44]	-	-	-0.93	-

* These correlation are shown in fig. 11.

The surface wax isolated the wood material from the exterior environment. However, in the lumen fill treatment with wax, the EMC and ASE did not changed.

High correlation between creep deflection vs. MOE_{st,4pb} could be expected, as the MOE_{st,4pb} was calculated from the (creep) deflection after 60 s. In actual fact, two deflections were compared: the deflection after 60 s (under a short-term load) and the deflection after 6 weeks with five wet and dry cycles under a sustained load.

The short-term deformation (MOE_{st,4pb} or MOE_{dyn}) is moderate to significantly correlated to the long-term creep deflection. This indicates that measuring the stiffness of a structural member, it should be possible to predict roughly its long-term performance under load.

In both moistening process, the results of this study confirm the suggestions from the literature, where the main correlation fitted (moderate up to significantly) for untreated pinewood (Epmeier 2006; Bengtsson 2001).

The lumen fill treatment (TEOS) had no effect on the MSE, however had shown the best correlation (moderate up to significant) with different variables.

The correlations shown by MMF resin (i2, high concentration) are not confirmed by DMDHEU treatment.

Creep deflection and stiffness had shown the best correlations. Moderate up to significant for control and TEOS treatments, except for resin based treatments with high concentration.

For cell wall treatments (DMDHEU and MMF resins) any clear pattern can be drawn for relative creep.

Epmeier (2006) with treated full scale specimens 1 : 1 with cell wall treatments (acetylation, MMF resin and thermowood in oil bath) under MSE had shown significant correlation for MOE_{dyn}, Density and creep deflection. However they were not confirmed with relative creep vs. MOE_{stat} and in furfurylated wood specimens. In the same works, controls and MMF treatments had shown the best correlations.

In figure 8, scatter plots for the correlations between creep deflection (on the x-axis) and MOE_{st,4pb} (on the y-axis) are shown. The corresponding coefficients of correlation can be found in table 3 (Creep deflection vs. MOE_{st,4pb}).

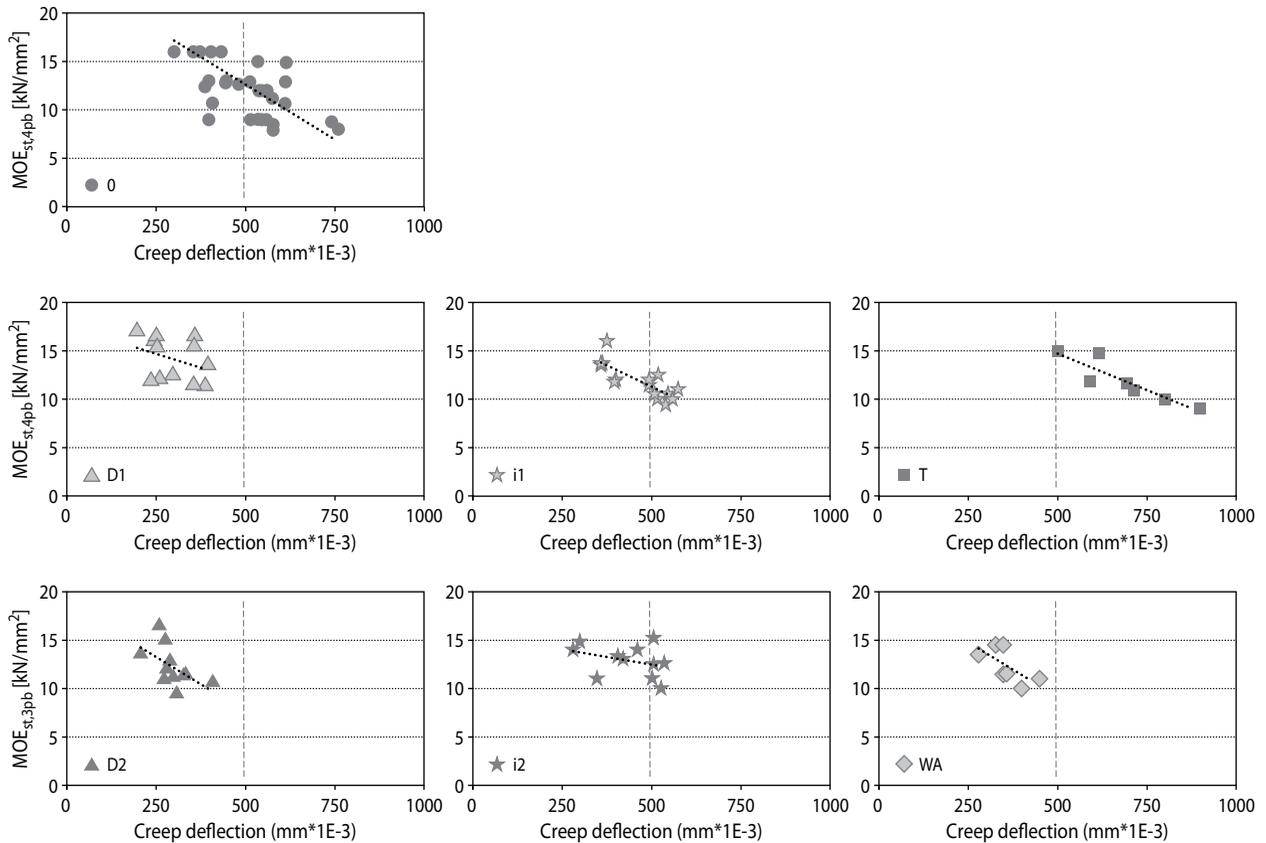


Fig. 8. Correlation scatter plots between creep deflection [mm] and $MOE_{st,4pb}$ [kN/mm² or GPa] under SL of 12 Nmm⁻² over a period of 42 days/1000 h. For abbreviations see the material item

In the lumen fill treatments (TEOS and wax) significant values were found and untreated pinewood had shown moderate correlation.

In the cell wall treatments (DMDHEU and MMF resin, medium concentration) moderate correlation were found (not significant). It seems that for high concentration in the resin based treatments, the correlation disappeared.

The control and lumen fill treatments (TEOS and wax) were correlated better than the cell wall modified specimens (DMDHEU and MMF resins).

Anti-creep efficiency (ACE)

The effect of chemical treatments on the MSE of wood can be characterized by the anti-creep efficiency (ACE) factor, which quantifies the ability of the treatment to reduce the MSE. The higher value for ACE, larger the reduction in creep is (Norimoto et al. 1992).

Figure 9 shows the ACE for all modification methods in both moistening process. The lumen fill treatment TEOS had shown lower ACE, near null (in the compression moistening a negative result was founded, whilst for tension moistening process a positive up to +9% was found). No effect in bending creep deflection by TEOS treatment is consistent with ASE and SSE, although both latter properties expressed different behaviour at itself.

Wax treatment was shown a particular behaviour and the high ACE presented was a surprise and in the other way around than ASE and SSE. The wax acts as a hurdle to the moisture change.

The wax effect in the lumen fill treatment clearly reduced the capillary water uptake in a ratio of 5 : 1 (Scholz et al. 2009). Similar results was found by Ranta-Maunus and Korttesmaa (2000) with full scale beams 1 : 1 under service conditions with surface coating with

alkyd paint. Santos (2009) suggested that glulam beams 1 : 1 with protected surface creep less.

The most effective modification were cell wall treatments, where DMDHEU performed best than MMF resin and different concentrations of resins did not shown significant different ACE.

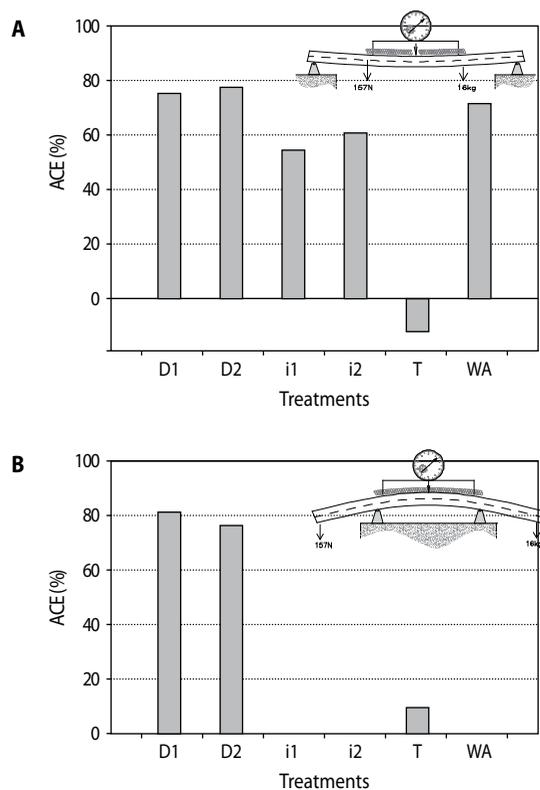


Fig. 9. Anti-creep efficiency (ACE) for compression – A and B – tension zone moistening. For abbreviations see material item

Few references in bending creep of modified wood are found. A summary is present in the table 4.

Although different setup to access the MSE has been used, ACE in acetylation and heat treatment wood specimens presented by different authors were comparable (Norimoto et al. 1992; Epmeier et al. 2005). The furfurylation treatment is roughly similar to the cell wall treatment DMDHEU (D2, with high concentration, 2.3 M). In this study, cell wall treatments (DMDHEU and MMF resins) had shown comparable ACE as furfurylated and MMF resins in Epmeier et al. (2007).

Relating ACE to changes in MC or Δ MC, in order to predict the effect of modification on the reduction in creep behaviour does not seem feasible (Epmeier et

al. 2007). The resin based treatments (DMDHEU and MMF) had shown different extend reduction in EMC, with 40% and 20% in wet or dry conditions for both types of resin, respectively. Any correlation between ACE presented in this study and the EMC or DEMC were found, despite the DMDHEU had shown best performance than MMF resin in ACE, EMC and DEMC. In general for cell wall treatments, the extent of ACE is in the same trends than the extent of change in ASE. The higher the ASE, higher the ACE is. However, modifications that lead to high ASE and to negative ACE at the same time may exist. Etherification with propylene oxide and polyethylene glycol impregnation are some examples presented by Norimoto et al. (1992).

Tab. 4. Weight percent gain (WPG), anti-swelling efficiency (ASE) and anti-creep efficiency (ACE) of different modification methods

Treatment	WPG [%]	ASE [%]	ACE [%]	Authors
Acetylation	23	66	48	Norimoto et al. 1992
Acetylation	13	70	53	Epmeier et al. 2004, 2005
HT* (180°C/3–10 h)	-2.4/-3.5	11/17	16/22	Norimoto et al. 1992
HT** (160/190°C)	–	–	22/25	Epmeier et al. 2007
MMF 7.5%	10	–	59	Epmeier et al. 2005
Phenol Resin	13	30	47	Norimoto et al. 1992
MMF 15%	16	–	64	Epmeier et al. 2006
i1 MMF 15%***	16	30	53/–	In this study
DMDHEU (1.3M)***	18	45	75/81	In this study
Furfurylation (F)	35	67	58	Epmeier et al. 2004, 2007
DMDHEU (2.3M)***	36	60	77/76	In this study
i2 MMF 30%***	39	38	61/–	In this study

* Heat treatment with the same temperature and different times, 3 and 10 hours; ** Heat treatment in vegetable oil bath; *** ACE values found with moistening process in compression and tension zone in bending

CONCLUSIONS

The results of this study with Portuguese untreated and modified wood in small scale (1 : 10) seem to fit with the results found in literature, with less scale 1 : 15 by Norimoto et al. (1992) and higher scale 1 : 1 by Epmeier et al. (2005) and Epmeier et al. (2007).

It can also conclude that the aims of the present study were fulfilled. Knowledge about the MSE in bending creep along the grain was acquired for modified wood with DMDHEU, MMF, TEOS and amid wax and untreated wood.

Relative creep after 42 days/1000 hours appears to be clear identified with this setup.

Untreated wood and lumen fill treatment with TEOS presented no creep limit. On the other hand, MSE of the modified wood with resins had shown a creep limits and generated stable displacement amplitude.

Cell wall modified wood (DMDHEU and MMF resin) decreased significantly the creep deflection, relative creep and enhanced the homogeneity of the creep results.

Lumen fill treatment with TEOS had no effect in the creep deflection.

From the correlations studied here, MOE_{dyn} has the best chance of becoming a functional indicator of relative creep. However, to prove this, a much broader statistical base is needed to enhance the significance of this correlation.

The density for modified wood cannot be used to predict any performance in creep in the same way as they can for untreated wood.

The effect of wood modifications on mechano-sorptive creep has been characterized by the anti-creep efficiency (ACE) factor, analogous to anti-swelling efficiency (ASE). However, only in the cell wall treatments (DMDHEU and MMF resin) were found a good correlation between ASE and ACE.

The change of the equilibrium moisture content imparted by the modification, mainly in the cell wall treatments, did not correlate well with creep results.

Modification of the cell wall and not filling the lumen alone is required to affect MSE in bending creep.

The creep behaviour depends more of the material relation with wet and dry environment than the enhanced mechanicals strength imparted by modification on the wood material. The former are translated by the

physical and mechanicals properties of the wood material, as ASE and SSE. The latter are translated by the increasing of compression strength and decreasing in tension strength, in general.

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